

Calculations

Annual energy consumption (kWh/a) , T average (°C) :

$$E_{\text{daily}} = P \times 24 + \frac{\Delta E_{df} \times 24}{\Delta t_{df}} \quad (2)$$

Where

E_{daily} is the energy in Wh over a period of 24 h

24 is h/d

P is the **steady state** power in watt for the selected **temperature control setting** as per Annex B.

ΔE_{df} is the representative incremental energy for **defrost and recovery** in Wh in accordance with Annex C (see C.5).

Δt_{df} is the estimated **defrost interval** in hours in accordance with Annex D.

Where there are additional defrost systems (each with its own **defrost control cycle**), the value of term based on ΔE_{df} and Δt_{df} is also added in Formula (2) for each additional defrost system.

$$T_{\text{average}} = T_{ss} + \frac{\Delta T h_{df}}{\Delta t_{df}} \quad (3)$$

Note : EN 60552-3:2020 , 6.8.2 clause, Equation 2-3 ,

Annual Energy , Daily energy consumption at 16 °C/ 32°C (kWh/24h) :

$$AE = 365 \times E_{\text{daily}}/L + E_{\text{aux}} \quad E_{\text{daily}} = 0,5 \times (E_{16} + E_{32})$$

Note : EN 60552-3:2020 , 6.8.2 clause, Equation 4,(EU) 2019/2019 Ecodesign Requirements Directive

Standard annual energy consumption (kWh/a)

SAE, expressed in kWh/a and rounded to two decimal places, is calculated as follows:

$$SAE = C \times D \times \sum_{c=1}^n A_c \times B_c \times [V_c/V] \times (N_c + V \times r_c \times M_c)$$

The modelling parameters are set out in Table 4.

Table 4

The values of the modelling parameters per compartment type

Compartment type	r_c (°)	N_c	M_c	C
Pantry	0,35	75	0,12	between 1,15 and 1,56 for combi appliances with 3- or 4-star compartments (°), 1,15 for other combi appliances, 1,00 for other refrigerating appliances
Wine storage	0,60			
Cellar	0,60			
Fresh food	1,00			
Chill	1,10	138	0,12	
0-star & ice-making	1,20	138	0,15	
1-star	1,50			
2-star	1,80			
3-star	2,10			
Freezer (4-star)	2,10			

(°) $r_c = (T_c - T_a)/20$; with $T_c = 24^\circ\text{C}$ and T_a with values as set out in Table 3.

(°) C for combi appliances with 3- or 4-star compartments is determined as follows:

where fr_{cf} is the 3- or 4-star compartment volume V_p as a fraction of V with $fr_{cf} = V_p/V$:

— if $fr_{cf} \leq 0,3$ then $C = 1,3 + 0,87 \times fr_{cf}$;

— else if $0,3 < fr_{cf} < 0,7$ then $C = 1,87 - 1,0275 \times fr_{cf}$;

— else $C = 1,15$.

The compensation factors are set out in Table 5.

Table 5

The values of the compensation factors per compartment type

Compartment type	A _c		B _c		D			
	Manual defrost	Auto-defrost	Freestanding appliance	Built-in appliance	≤ 2 (*)	3 (*)	4 (*)	> 4 (*)
Pantry	1,00		1,00	1,02	1,00	1,02	1,035	1,05
Wine storage								
Cellar								
Fresh food								
Chill				1,03				
0-star & ice-making	1,00	1,10		1,05				
1-star								
2-star								
3-star								
Freezer (4-star)								

(*) number of external doors or compartments, whichever is lowest.

Note : (EU) 2019/2019 Ecodesign Requirements Directive, Clause 5, Table 4-5

5. Determination of the EEI:

EEI, expressed in % and rounded to the first decimal place, calculated as:

$$EEI = AE/SAE.$$

Note : (EU) 2019/2019 Ecodesign Requirements Directive, Clause 5

Auxiliary energy (kWh/a)

$$W_{heaters} = \left[\sum_{i=1}^k (R_i \times P_{H_i}) \right] \times 1,3 \quad (40)$$

Table F.1 — Format for temperature and humidity data – Ambient controlled anti-condensation heaters

Relative Humidity	RH band mid-point	Probability R _i at 16 °C	Probability R _i at 22 °C	Probability R _i at 32 °C	Heater W at 16 °C	Heater W at 22 °C	Heater W at 32 °C
0 to 10 %	5 %	0,00 %	0,00 %	0,34 %	P _{H1}	P _{H11}	P _{H21}
10 to 20 %	15 %	0,61 %	6,86 %	2,01 %	P _{H2}	P _{H12}	P _{H22}
20 to 30 %	25 %	3,11 %	14,57 %	1,61 %	P _{H3}	P _{H13}	P _{H23}
30 to 40 %	35 %	5,03 %	14,83 %	0,86 %	P _{H4}	P _{H14}	P _{H24}
40 to 50 %	45 %	5,09 %	11,67 %	0,18 %	P _{H5}	P _{H15}	P _{H25}
50 to 60 %	55 %	4,67 %	8,31 %	0,01 %	P _{H6}	P _{H16}	P _{H26}
60 to 70 %	65 %	3,39 %	5,54 %	0,00 %	P _{H7}	P _{H17}	P _{H27}

Relative Humidity	RH band mid-point	Probability R _i at 16 °C	Probability R _i at 22 °C	Probability R _i at 32 °C	Heater W at 16 °C	Heater W at 22 °C	Heater W at 32 °C
70 to 80 %	75 %	3,17 %	2,51 %	0,00 %	P _{H8}	P _{H18}	P _{H28}
80 to 90 %	85 %	2,85 %	0,66 %	0,00 %	P _{H9}	P _{H19}	P _{H29}
90 to 100 %	95 %	2,05 %	0,07 %	0,00 %	P _{H10}	P _{H20}	P _{H30}

Note : EN 62552-3:2020, Annex F 2.5, Equation 40, Table F.1

Incremental defrost and recovery energy consumption at 16 /32 °C (Wh)

$$\Delta E_{df} = (E_{end-F} - E_{start-D}) - \frac{(P_{SS-D} + P_{SS-F})}{2} \times (t_{end-F} - t_{start-D}) \quad (19)$$

$$\Delta E_{df} = \frac{\sum_{j=1}^m \Delta E_{dfj}}{m} \quad (22)$$

Note : EN 62552-3:2020 Annex C, Clause C.3.3, Equation 19-22

Defrost interval at 16 /32 °C (h)

for Compressor Run Time Defrost Controller

$$\Delta t_{df} = \frac{\Delta t_{rt} - \Delta t_{dr} - \Delta t_{dh}}{CRt_{SS}} + \Delta t_{axy} \quad (26)$$

for Variable Defrost Controller

$$\Delta t_{df32} = \frac{\Delta t_{d-max} \times \Delta t_{d-min}}{[0.2 \times (\Delta t_{d-max} - \Delta t_{d-min}) + \Delta t_{d-min}]} \quad (27)$$

$$\Delta t_{df16} = 2 \times \Delta t_{df32}$$